

# Poiseuille flow



les hypothèses typiques de l'écoulement de Poiseuille: laminaire, établi, fluide incompressible

Ces conditions sont nécessaires pour que la **loi de Poiseuille** s'applique (débit, profil de vitesse, relation pression-viscosité, etc.).

### 1- Laminaire

Un écoulement « laminaire » signifie que les couches du fluide glissent les unes sur les autres sans mélange turbulent.

☐ Si une de ces hypothèses n'est pas vérifiée (par exemple un fluide compressible, un écoulement turbulent, ou un régime non-stationnaire), la loi de Poiseuille ne sera plus rigoureusement applicable, ou il faudra prendre en compte des corrections.

### 2- Établi (ou stationnaire)

•« Établi » veut dire que les propriétés du fluide (vitesse, pression...) ne varient pas dans le temps à un point donné :

l'écoulement est **permanent**. En régime établi, on peut faire des simplifications dans les équations de Navier-Stokes (par exemple, la dérivée temporelle disparaît).

•Cette hypothèse est essentielle pour la loi de Poiseuille : elle garantit que le débit est constant dans le temps.

Donc l'« établi » est bien une hypothèse classique.

### 3. Fluide incompressible

- L'incompressibilité signifie que la masse volumique  $\rho$  du fluide reste (pratiquement) constante pendant l'écoulement.

Beaucoup de liquides (comme l'eau) sont très bien modélisés comme incompressibles dans ces conditions.

- La loi de Poiseuille (Hagen-Poiseuille) suppose effectivement un fluide incompressible.

à partir des équations de Navier–Stokes) qui montre comment les hypothèses « laminaire, établi, incompressible » mènent à la loi de Poiseuille pour un tube circulaire droit.

#### Hypothèses et configuration

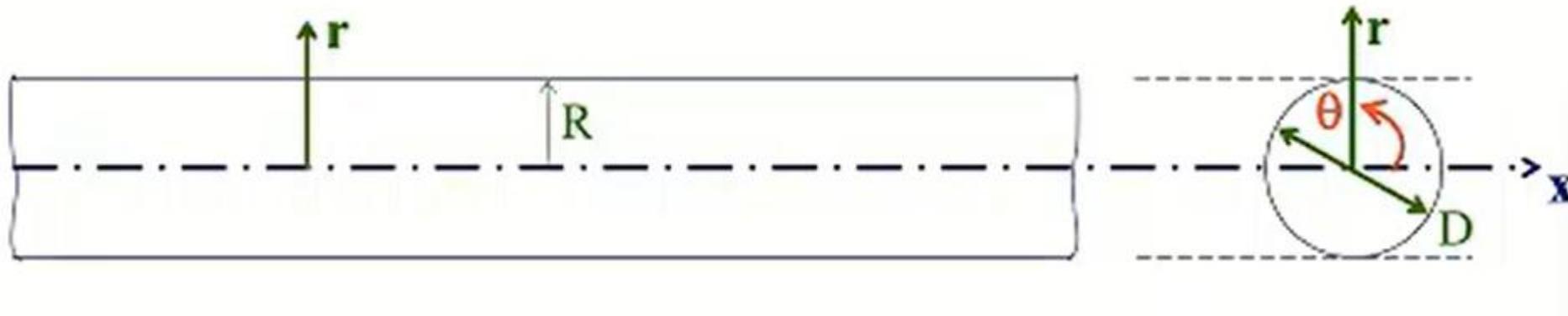
- Écoulement dans un tube droit de rayon  $R$  et longueur  $L$ .

- Coordonnées cylindriques  $(r, \theta, z)$  avec  $z$  axe axial.

- Fluide newtonien de viscosité dynamique  $\mu$  et incompressible.

- Écoulement **laminaire, axial, axisymétrique** (pas de dépendance en  $\theta$ ), et **établi** (stationnaire) — donc la vitesse n'a que la composante axiale  $u_z(r)$ , notée  $u(r)$ , et  $\partial/\partial t = 0$ .

- Pas de forces de volume (gravité négligée), conditions aux limites :  $u(R) = 0$  (no-slip),  $u$  finie en  $r = 0$



The velocity field of a fully developed flow:

- independent of time
- independent of the axial coordinate (identical in every straight section).

**Established:**

- independent of time
- independent of the axial coordinate

$$\begin{cases} (\partial V_i / \partial t) \equiv 0 \\ (\partial V_i / \partial x) \equiv 0 \end{cases}$$

In flows through cylindrical pipes, the velocity field is parabolic (paraboloid profile), which gives us symmetry with respect to the angle  $\theta$ ; this is what we call circular rotational symmetry. This symmetry is valid for both velocity and pressure.

**Revolution symmetry:**

$$\begin{cases} (\partial V_i / \partial \theta) \equiv 0 \\ (\partial p^* / \partial \theta) \equiv 0 \end{cases}$$

Let us use cylindrical coordinates (O, r,  $\theta$ , x) to write the Navier-Stokes equations and the Continuity equation.

### Continuity equation

$$\frac{1}{r} \frac{\partial(r V_r)}{\partial r} + \frac{1}{r} \frac{\partial V_\theta}{\partial \theta} + \frac{\partial V_x}{\partial x} = 0$$

### Momentum equations

$$\left\{ \begin{aligned} \rho \left[ \frac{\partial V_r}{\partial t} + V_r \frac{\partial V_r}{\partial r} + \frac{V_\theta}{r} \frac{\partial V_r}{\partial \theta} + V_x \frac{\partial V_r}{\partial x} - \frac{V_\theta^2}{r} \right] &= -\frac{\partial p^*}{\partial r} + \mu \left\{ \frac{\partial}{\partial r} \left[ \frac{1}{r} \frac{\partial}{\partial r} (r V_r) \right] + \frac{1}{r^2} \frac{\partial^2 V_r}{\partial \theta^2} + \frac{\partial^2 V_r}{\partial x^2} - \frac{2}{r^2} \frac{\partial V_\theta}{\partial \theta} \right\} \\ \rho \left[ \frac{\partial V_\theta}{\partial t} + V_r \frac{\partial V_\theta}{\partial r} + \frac{V_\theta}{r} \frac{\partial V_\theta}{\partial \theta} + V_x \frac{\partial V_\theta}{\partial x} + \frac{V_r V_\theta}{r} \right] &= -\frac{1}{r} \frac{\partial p^*}{\partial \theta} + \mu \left\{ \frac{\partial}{\partial r} \left[ \frac{1}{r} \frac{\partial}{\partial r} (r V_\theta) \right] + \frac{1}{r^2} \frac{\partial^2 V_\theta}{\partial \theta^2} + \frac{\partial^2 V_\theta}{\partial x^2} + \frac{2}{r^2} \frac{\partial V_r}{\partial \theta} \right\} \\ \rho \left[ \frac{\partial V_x}{\partial t} + V_r \frac{\partial V_x}{\partial r} + \frac{V_\theta}{r} \frac{\partial V_x}{\partial \theta} + V_x \frac{\partial V_x}{\partial x} \right] &= -\frac{\partial p^*}{\partial x} + \mu \left\{ \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial V_x}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 V_x}{\partial \theta^2} + \frac{\partial^2 V_x}{\partial x^2} \right\} \end{aligned} \right.$$

Hypotheses of the study (Poiseuille flow):

**1. Steady flow:**

$$\begin{cases} \frac{\partial V_i}{\partial t} \equiv 0 \\ \frac{\partial V_i}{\partial x} \equiv 0 \end{cases} \quad i = (r, \theta, x)$$

**2. Revolution symmetry:**

$$\frac{\partial V_i}{\partial \theta} \equiv 0 \quad \frac{\partial p^*}{\partial \theta} \equiv 0$$

According to the hypotheses, the velocity depends only on  $r$ , so it varies only with  $r$ .

$$\Rightarrow \text{One-dimensional flow} \quad \mathbf{V}_i = V_i(\mathbf{r})$$

According to the Continuity Equation, the radial component of the velocity field is identically zero.

$$\frac{1}{r} \frac{\partial (r V_r)}{\partial r} + \cancel{\frac{1}{r} \frac{\partial V_\theta}{\partial \theta}} + \cancel{\frac{\partial V_x}{\partial x}} = 0 \quad \rightarrow \quad [r V_r(\mathbf{r})] = Cte$$

n.p.c.: non-penetration condition

C.L. : en  $r = R$ , on a :  $V_r(r = R) = 0$  (c.n.p)



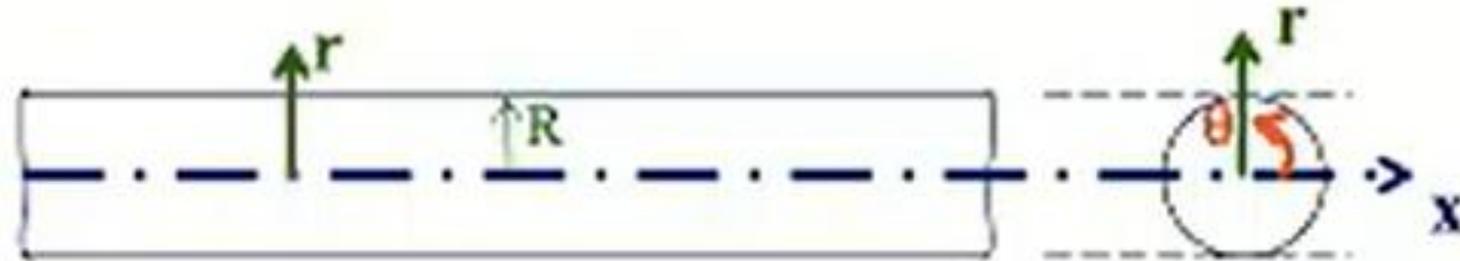
$$R V_r(R) = 0$$

$$\begin{array}{l} [r V_r(r)] = \text{Cte} \\ \text{Cte} = 0 \\ R V_r(R) = 0 \end{array}$$



$$V_r \equiv 0$$

Continuity equation  $\Rightarrow V_r = 0$



## Momentum equations

$$\left\{ \begin{array}{l} -\frac{\rho V_0^2}{r} = -\frac{\partial p^*}{\partial r} \\ 0 = \mu \frac{\partial}{\partial r} \left[ \frac{1}{r} \frac{\partial}{\partial r} (r V_0) \right] \\ 0 = -\frac{\partial p^*}{\partial x} + \mu \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial V_x}{\partial r} \right) \end{array} \right.$$

**Projection radiale (suivant  $r$ )**

**Projection tangentielle (sur  $\theta$ )**

**Projection axiale (suivant  $x$ )**

So the general properties of Poiseuille flow are:

**Steady flow:**

$$\left\{ \begin{array}{l} (\partial V_i / \partial t) \equiv 0 \\ (\partial V_i / \partial x) \equiv 0 \end{array} \right.$$

$$V_i = V_i(r)$$

**One-dimensional flow**

**Revolution symmetry:**

$$\left\{ \begin{array}{l} (\partial V_i / \partial \theta) \equiv 0 \\ (\partial p^* / \partial \theta) \equiv 0 \end{array} \right.$$



$$V_r \equiv 0$$

$$V_\theta \equiv 0$$

**Uni-directional flow**

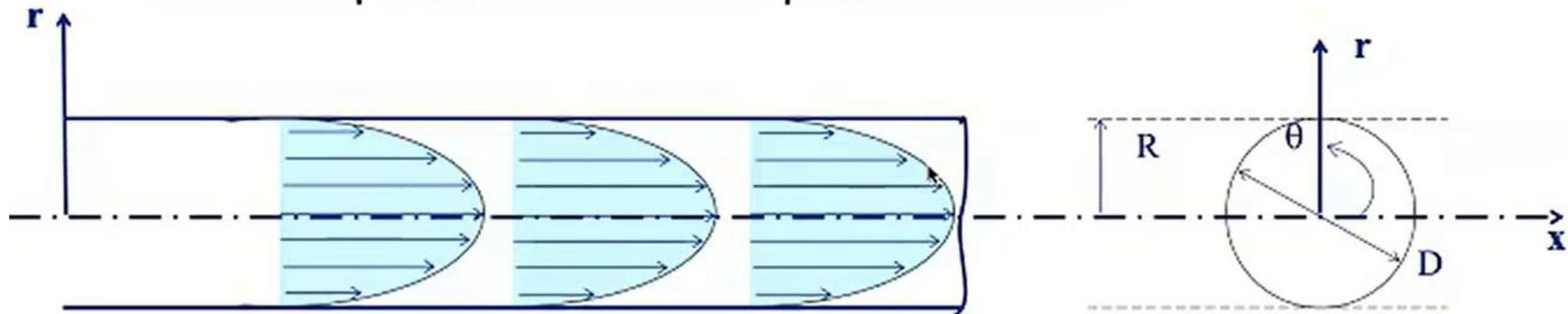
$$\begin{array}{l}
 \text{Projection radiale (suivant } r) \\
 \text{Projection tangentielle (sur } \theta) \\
 \text{Projection axiale (suivant } x)
 \end{array}
 \left\{ \begin{array}{l}
 0 = -\frac{\partial p^*}{\partial r} \\
 0 = -\frac{\partial p^*}{\partial \theta} \\
 0 = -\frac{dp^*}{dx} + \mu \frac{1}{r} \frac{d}{dr} \left( r \frac{dV_x}{dr} \right)
 \end{array} \right. \quad p^* = p^*(x)$$

The pressure is uniform over the entire cross-section, i.e., it varies only along the x-direction.

Finally, here is the velocity profile in a straight cylindrical pipe, far from the inlet, when the fluid is incompressible, Newtonian, isothermal, and flows in a fully developed regime.

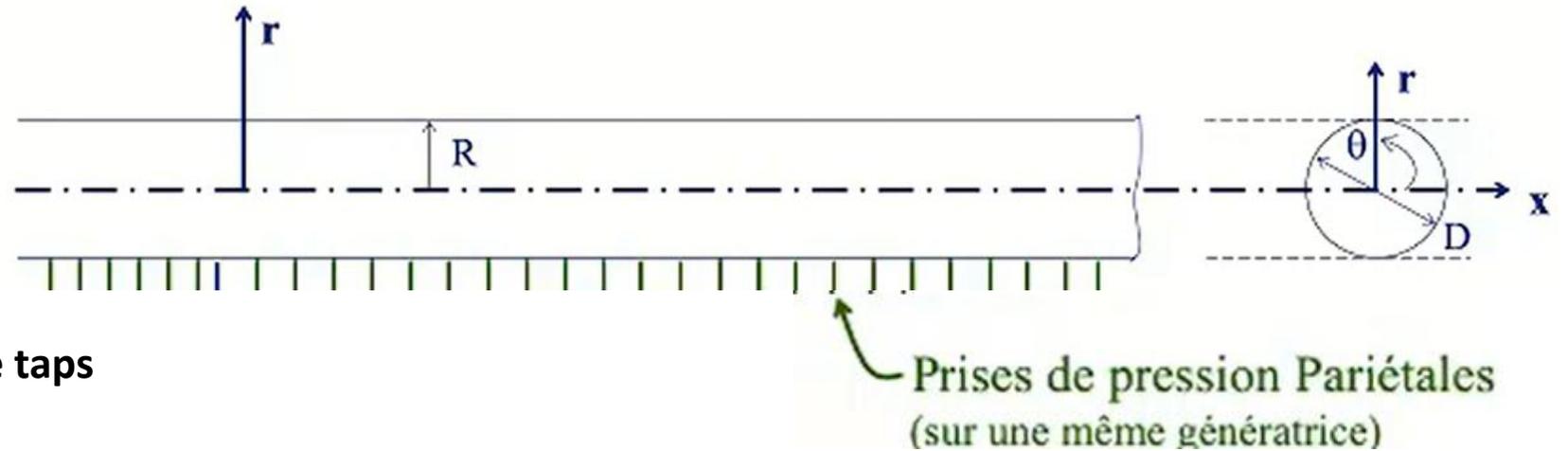
$$V_x(r) = \frac{1}{4\mu} \frac{dp^*}{dx} (r^2 - R^2)$$

The profile is parabolic far from the inlet because the flow is fully developed ; therefore it is the same parabola since the velocity is constant along x ( $\frac{dV_i}{dx} = 0$ );



## How can we experimentally demonstrate that the flow is established (or fully developed)?

- This means proving that **the velocity profile no longer changes in the direction of flow**. One of the simplest and most common methods **is indeed to use wall pressure taps**.



### Experimental method: wall pressure taps

#### Principle:

Several pressure taps are installed along the wall of a conduit (for example, a pipe) at regular distances from the inlet, and the static pressure  $P(x)$  is measured at these points.

#### Expected observation:

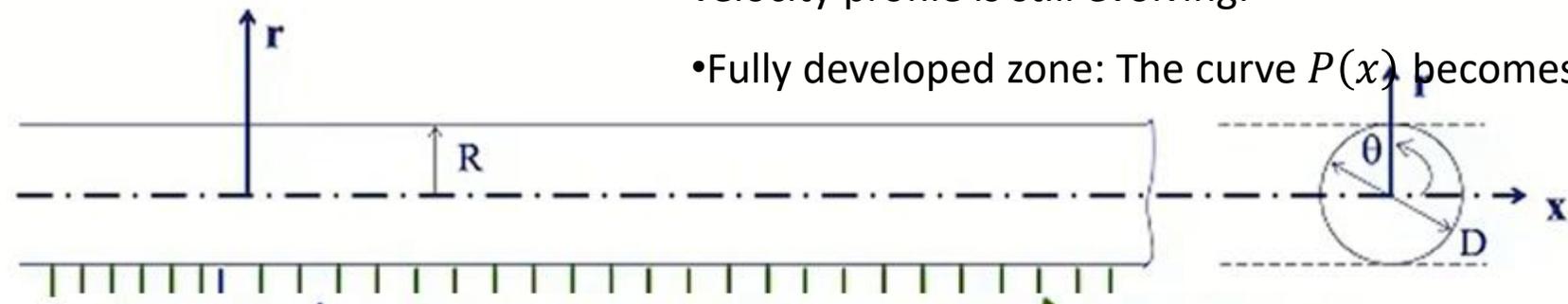
- In the steady regime, the head loss (pressure drop) becomes linear with the distance  $x$ .
- In other words, the slope  $\frac{dP}{dx}$  becomes constant.
- This linearity means that **the velocity profile no longer changes**, because resistance to movement (viscosity) is balanced by a constant pressure gradient.

•Entry zone (not fully developed): The pressure drop varies in a non-linear way because the

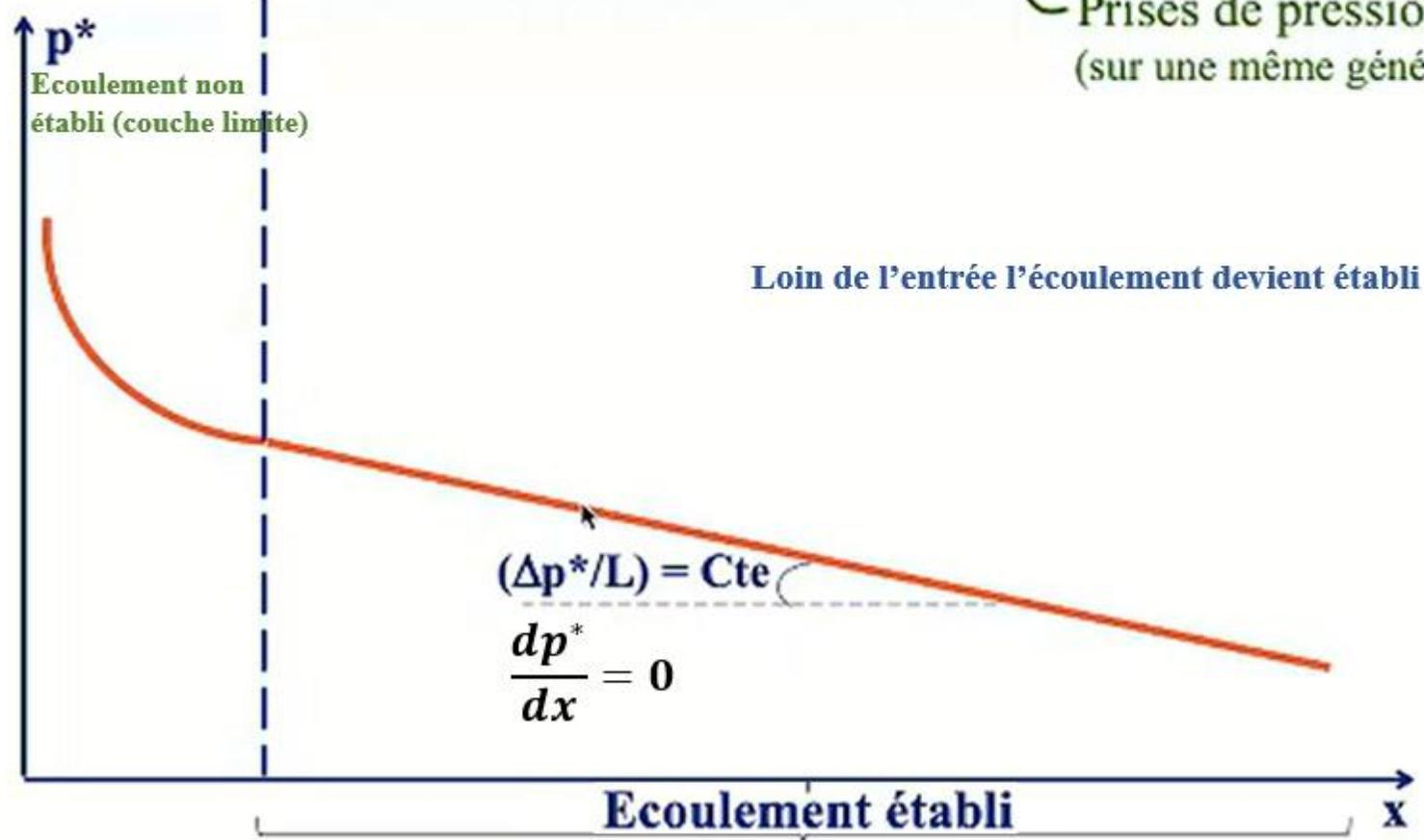
velocity profile is still evolving.

•Fully developed zone: The curve  $P(x)$  becomes straight, indicating fully developed flow.

How to interpret the measurements:



Prises de pression Pariétales  
(sur une même génératrice)





### Typical experimental illustration:

1. Use a differential manometer between two successive pressure taps.
2. Record  $\Delta P$  (pressure difference) between these taps at different positions.
3. Plot  $\Delta P$  as a function of the distance between the taps.
4. Identify the region where  $\Delta P$  becomes proportional to the distance—this is the fully developed zone.



### Remark:

It is also possible to experimentally validate fully developed flow by measuring the velocity profile. The main methods cited are:

- Using a Pitot tube (noted as more delicate).
- Using anemometry (for example, hot-wire anemometry), although these techniques are more complex and costly.